

Wind-induced response of slender suspension bridges:

Full-scale measurements on the Hardanger Bridge



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Introduction

- Interconnected with the E39 project
- Suspension bridges are considered for many connections
- Long-span and super long-span bridges (expensive, credibility at stake)
- Validate models, methods
- How well we can predict the response?
- Unexpected behavior?
- Monitoring of existing structures → good start

Hardanger Bridge

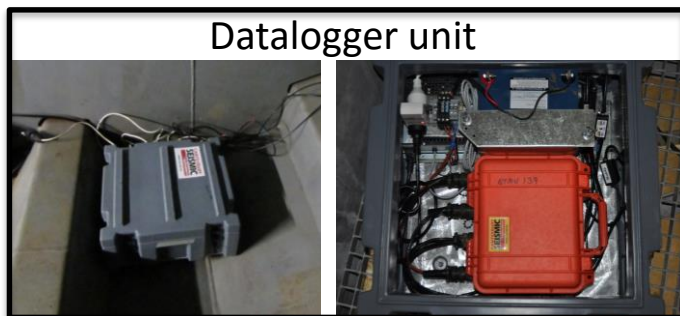
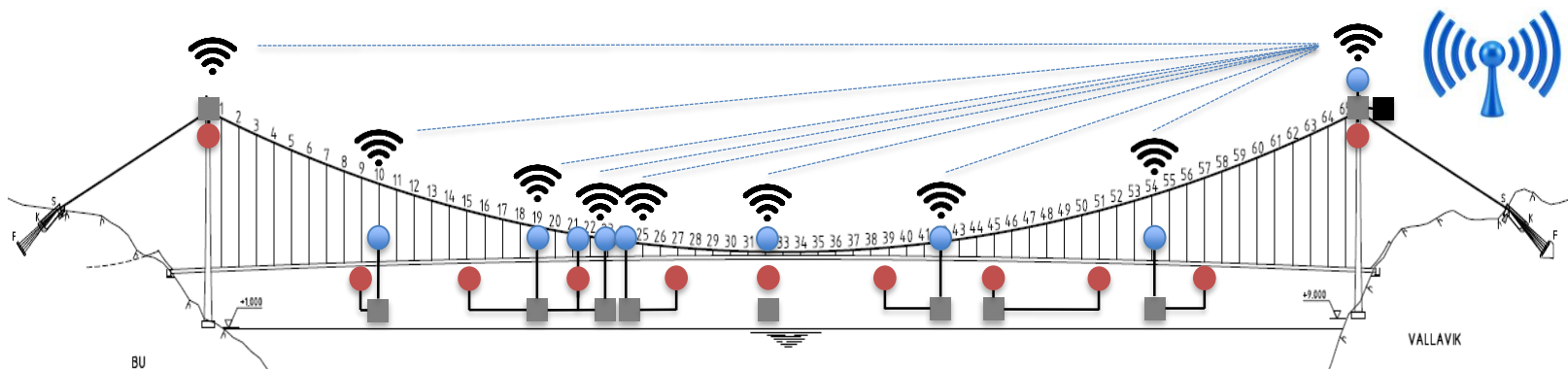
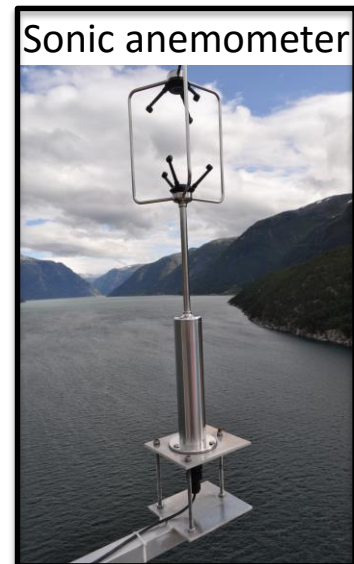


- Opened in 2013 (modern design)
- Main span is 1310 meters (longest in Norway)
- Complex terrain (fjord), Mountains of 1000~1500 m
- Slender deck (18 meters wide)
- Strong winds !

Monitoring wind speeds & accelerations along the bridge!

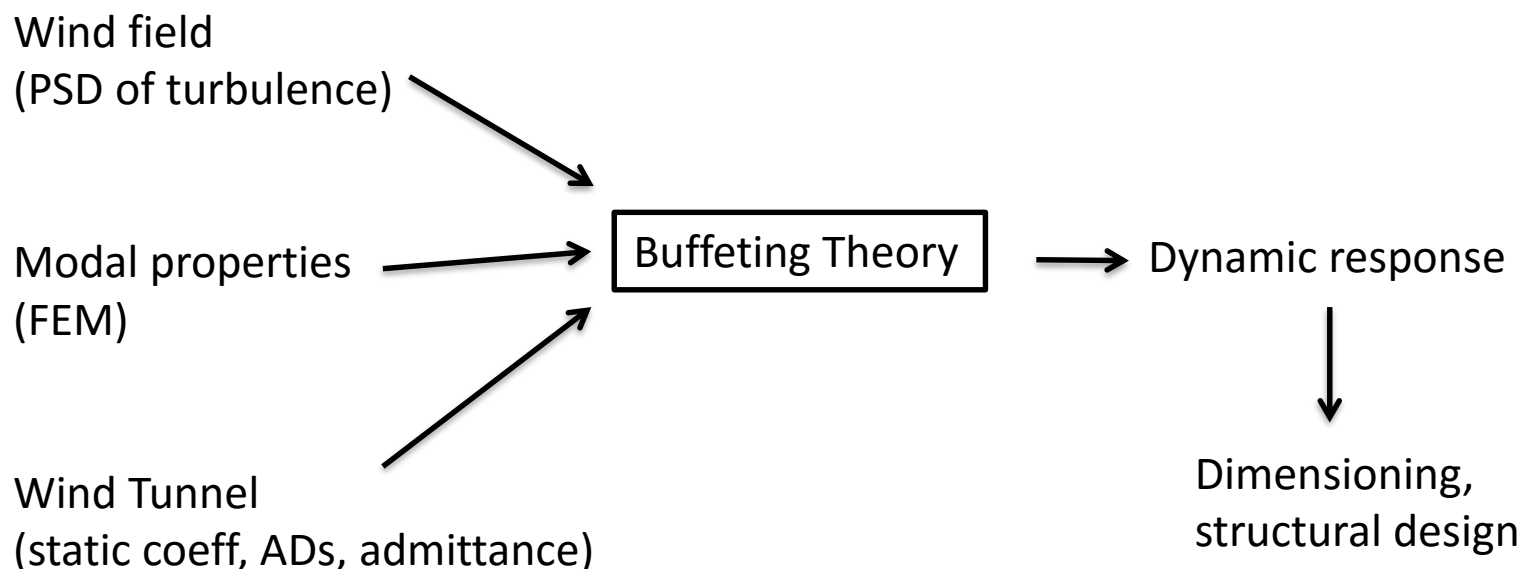
Measurement System

- 20 accelerometers
- 9 anemometers
- 11 dataloggers
- 10 wireless antennas



Design of suspension bridges against wind actions

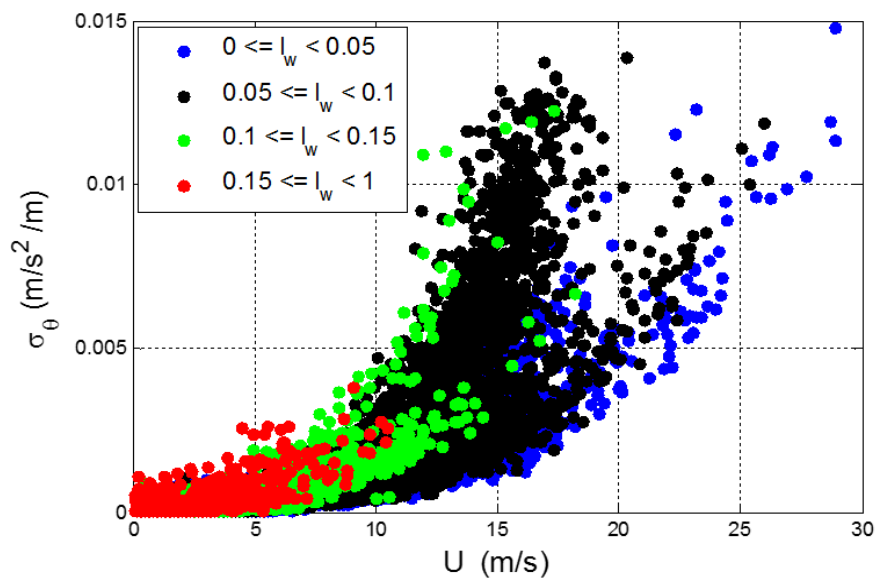
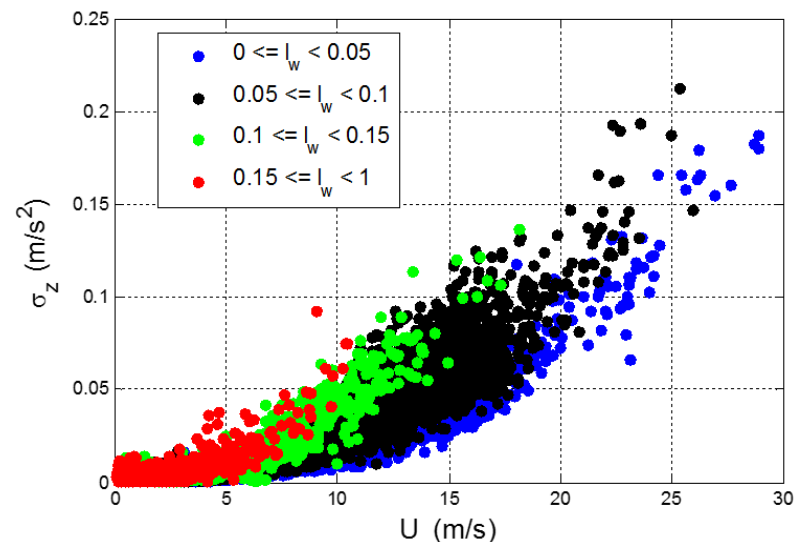
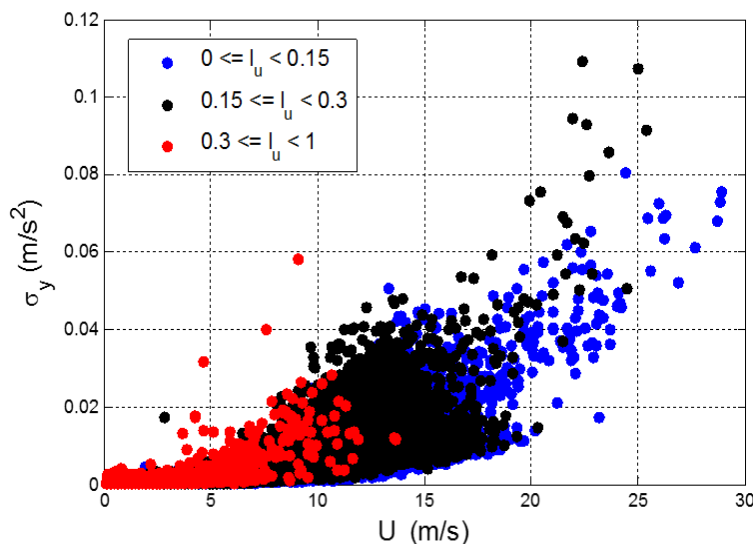
- Buffeting loading



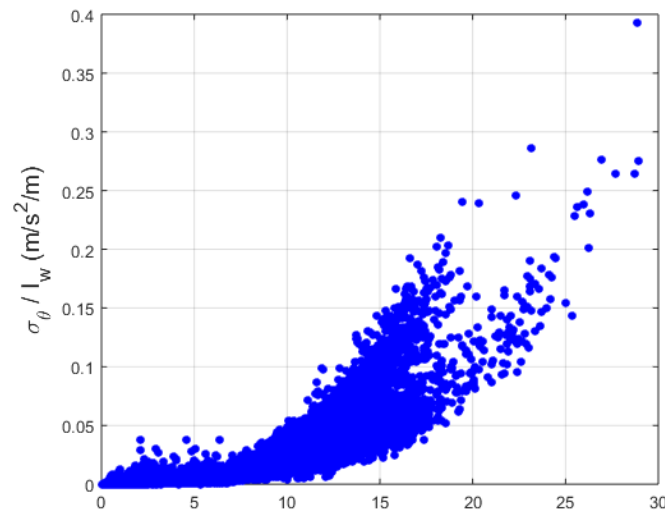
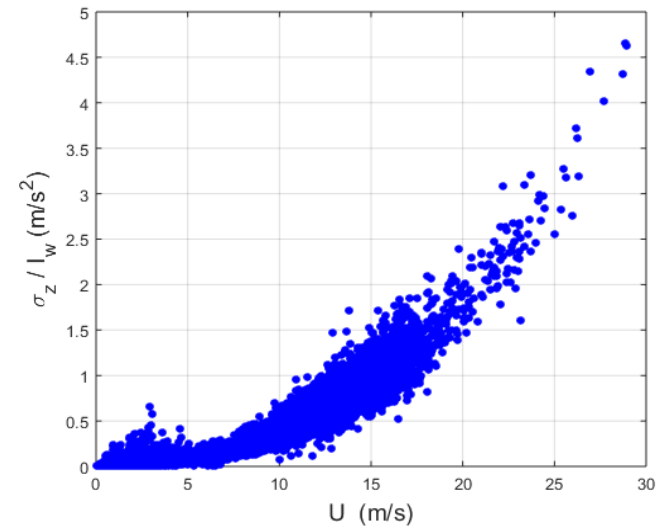
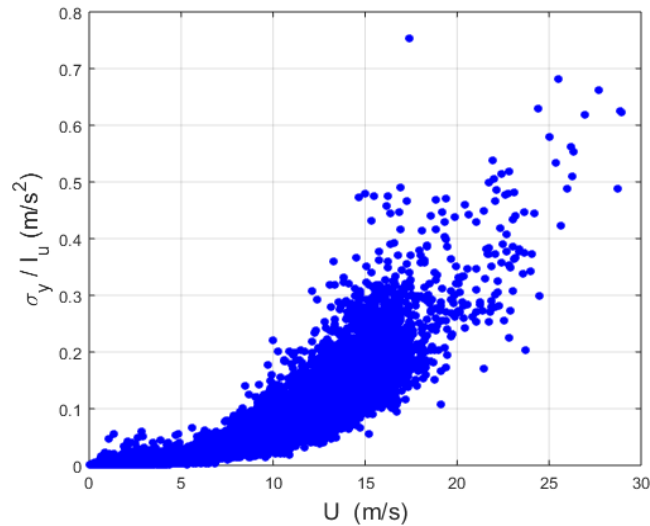
Design of suspension bridges against wind actions

- N400 – Norwegian Handbook for Bridge Design
 - Wind Characteristics (for spans > 300 m \rightarrow field measurements)
 - Mean wind speed (design parameter)
 - Turbulence intensity
 - Length scales
 - One-point spectra
 - Root coherence
- } Deterministic!
(functions of height, mean speed)

Buffeting Response of the Hardanger Bridge

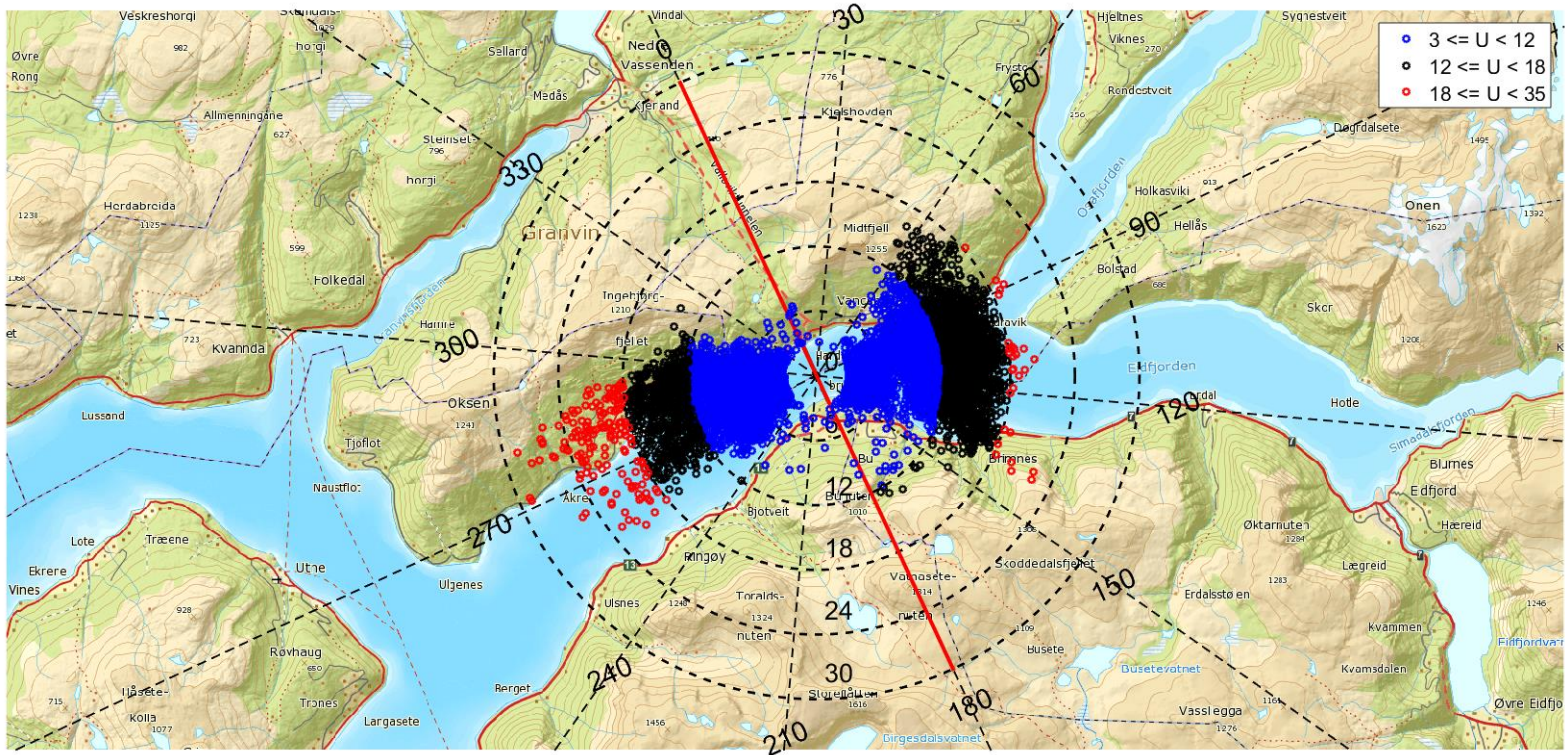


Buffeting Response of the Hardanger Bridge



Wind Characteristics

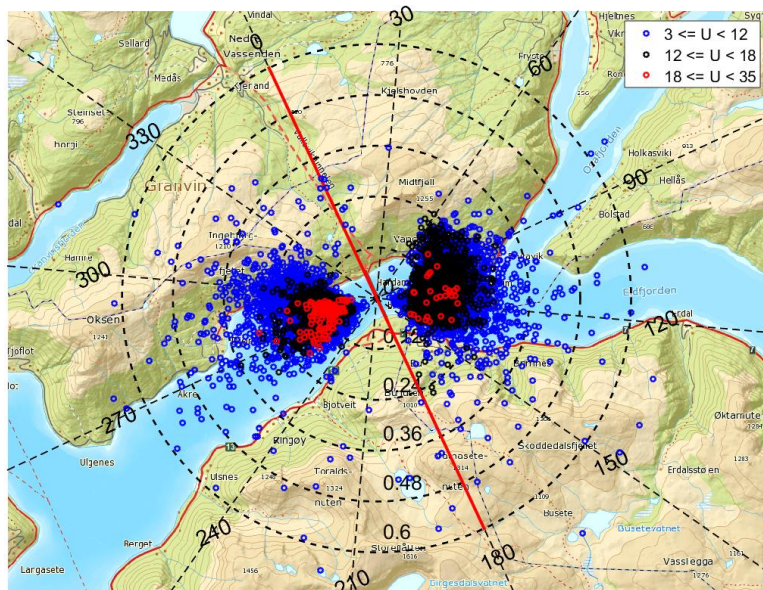
- 10-min mean wind speed (m/s)



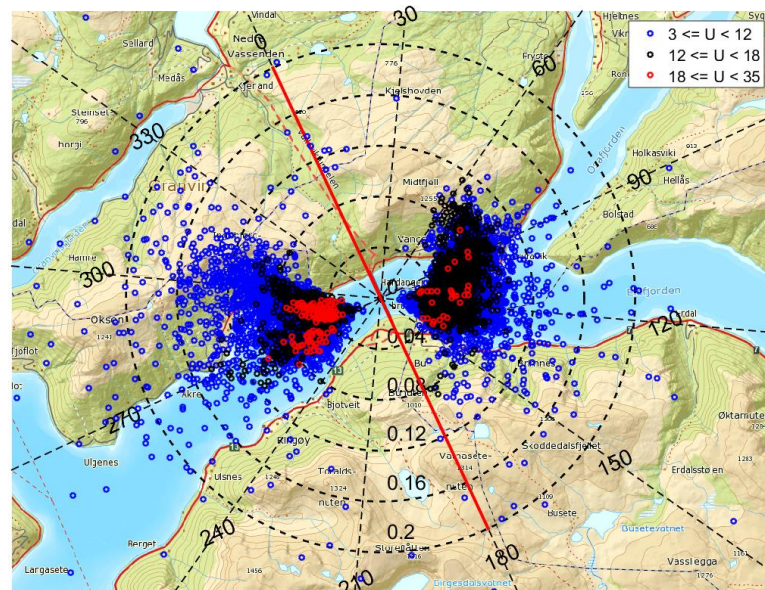
Wind Characteristics

- Turbulence Intensity

Along wind



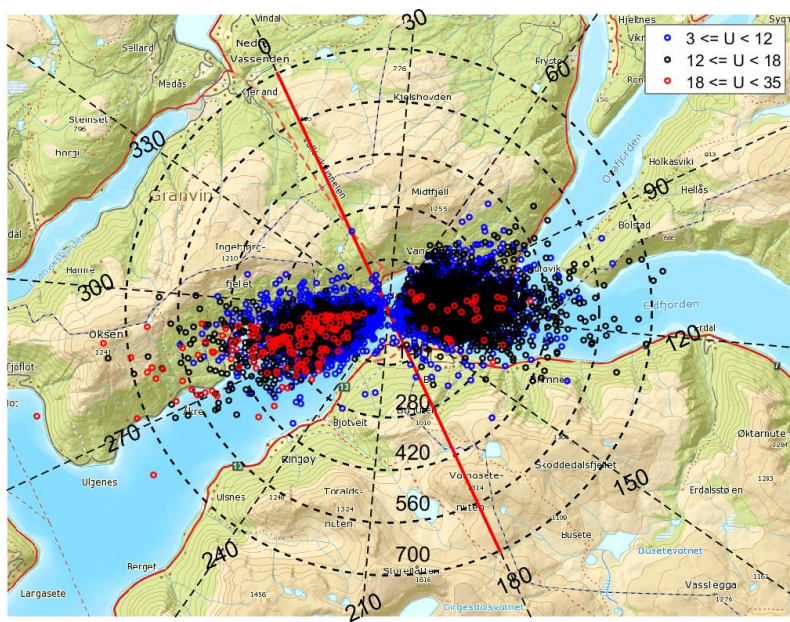
Vertical



Wind Characteristics

- Length scales (m)

Along wind



Response Surface Analysis

- Linear regression

- Quadratic surface
$$y = \beta_0 + \sum_{i=1}^n \left(\beta_i x_i + \sum_{j=i+1}^n \beta_{ij} x_i x_j + \beta_{ii} x_i^2 \right)$$

- Estimate coefficients by least squares

Predictor variables:

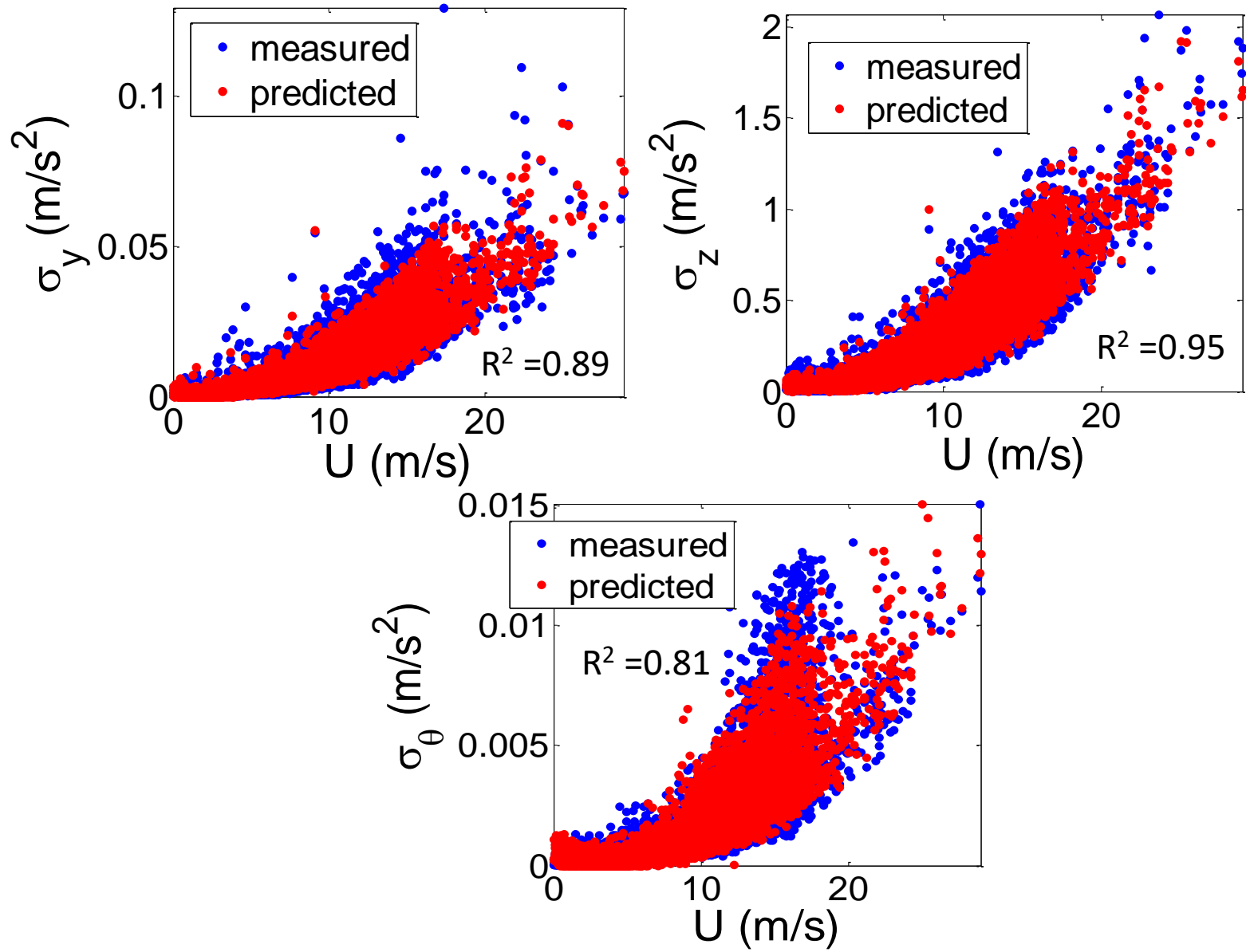
- *mean wind speed (U)*
- *turbulence standard deviations (u, v, w)*
- *length scales (u, w)*
- *wind yaw-angle*
- *angle-of-attack*
- *standard deviation of U along the bridge*



RMS Response

- *Lateral*
- *Vertical*
- *Torsional*

Response Surface Analysis



Response Surface Analysis

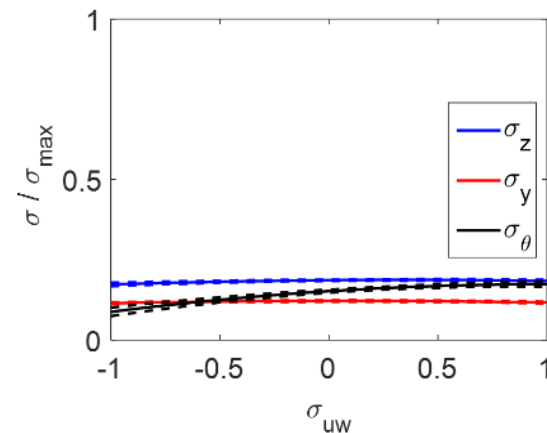
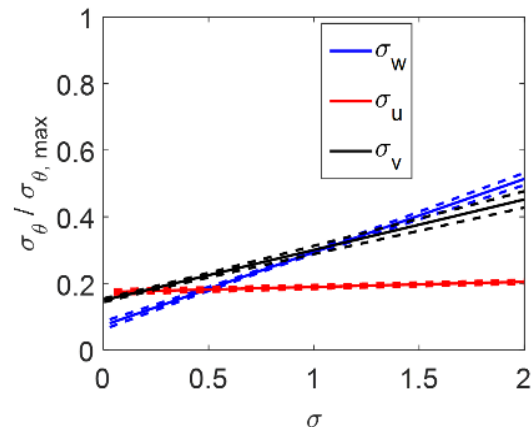
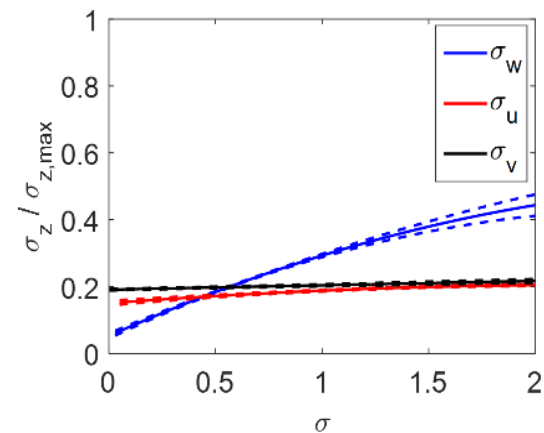
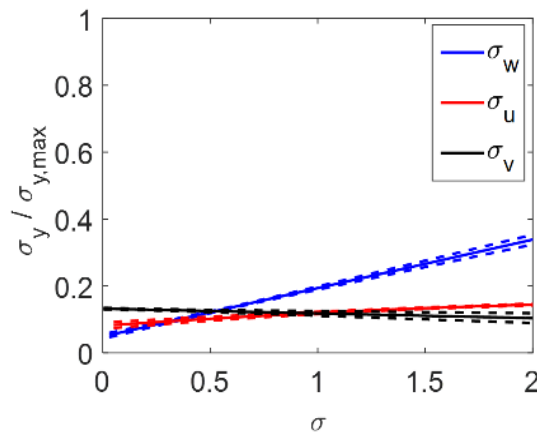
- Importance of wind-related variables: Hypothesis testing ($H_0: \beta = 0$)

Significance of terms in response surface analyses

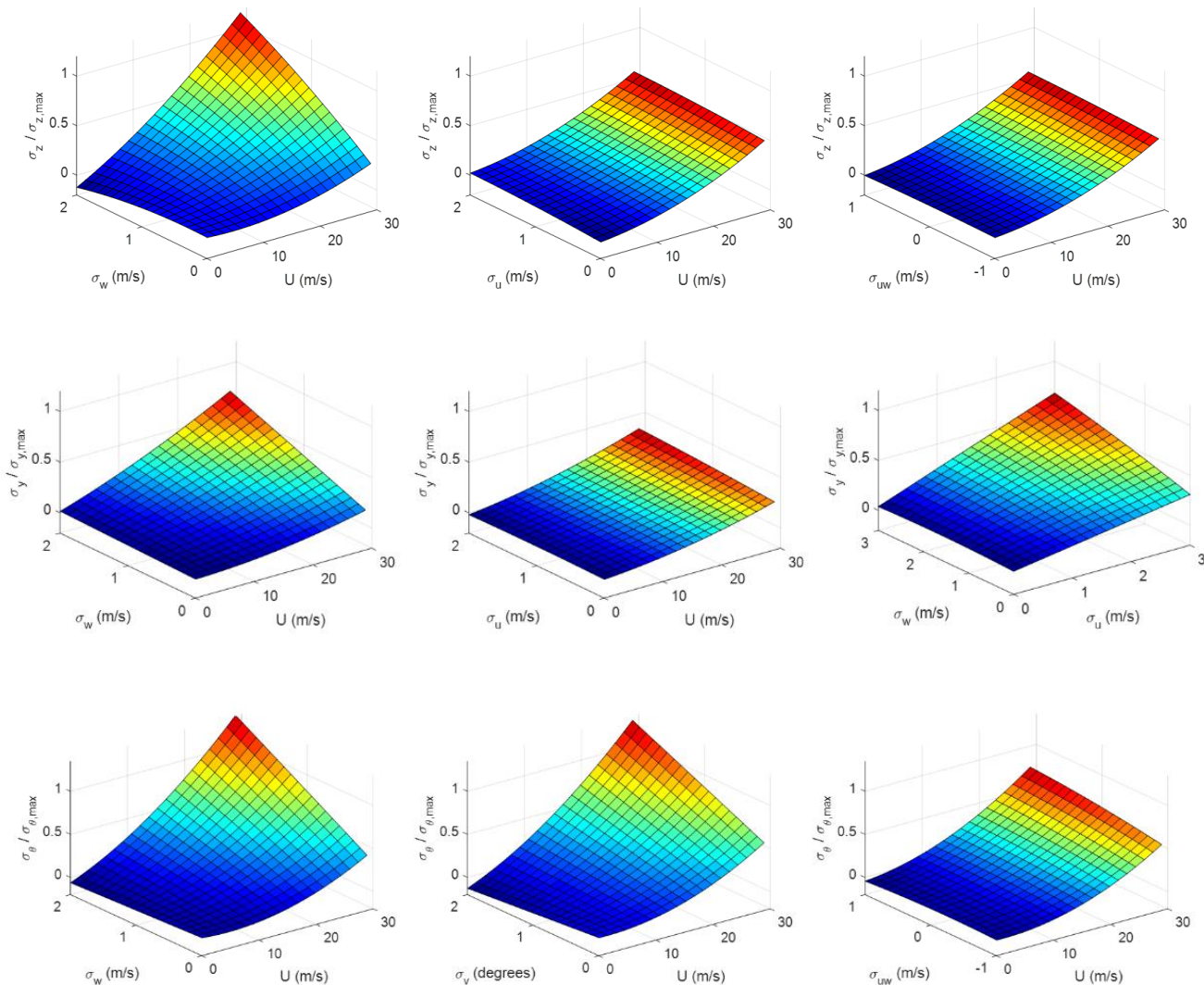
Vertical acceleration		Lateral acceleration		Torsional acceleration	
Term	p-value	Term	p-value	Term	p-value
U	0	U. σ_w	1.96E-58	U	0
U. σ_w	6.85E-214	L _w	3.03E-51	U. σ_w	1.51E-234
U ²	2.60E-137	σ_w . σ_u	2.82E-41	U. σ_v	2.49E-169
L _w	9.47E-90	U ²	2.34E-32	U ²	3.08E-147
σ_{ms}	9.01E-48	α_{yaw} . σ_u	2.36E-27	U. α_{yaw}	5.15E-93
σ_{uw}^2	9.25E-28	σ_w . L _w	7.09E-25	L _w . σ_v	6.76E-67
σ_u	1.01E-26	σ_w . σ_{ms}	1.37E-20	σ_w . L _u	3.02E-64
L _w ²	6.27E-21	α_{yaw} . σ_v	2.22E-20	σ_{uw}^2	1.88E-47
σ_w . L _u	1.32E-19	σ_{uw}^2	4.11E-20	α_{yaw}	1.08E-33
α_{yaw} . σ_u	1.23E-17	U. β	9.79E-20	α_{yaw} . L _u	9.20E-29
σ_w . σ_v	4.08E-16	σ_w . L _u	3.09E-17	U. L _w	7.18E-19
σ_u . L _u	9.53E-16	L _w ²	7.43E-13	σ_u . L _w	8.32E-17
σ_w . L _w	2.90E-15	α_{yaw} . L _u	1.11E-11	U. σ_{uw}	1.61E-15
σ_u^2	1.64E-13	σ_u^2	2.15E-11	L _w ²	5.62E-15
σ_w . α_{yaw}	2.24E-13	σ_u . σ_{uw}	1.43E-10	α_{yaw}^2	4.30E-13
σ_w . σ_u	3.14E-13	U. σ_u	5.69E-10	σ_{uw} . L _w	2.04E-12

Response Surface Analysis

- Mean speed \rightarrow most important ($R^2 \sim 60-70\%$)
- Turbulence



Response Surface Analysis

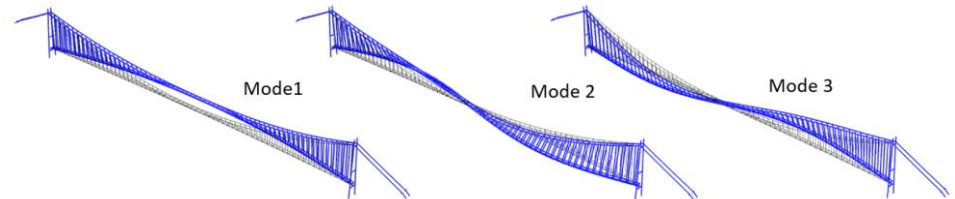


Response Surface Analysis

- Other parameters
- Yaw-angle → similar response levels in skew and perpendicular winds
- Angle-of-attack → no significant correlation is observed
- Length scales → vertical component!

Analytical Prediction of the Buffeting Response

- Multimode theory
- Frequency domain
- Mode shapes from FEM (Abaqus model)

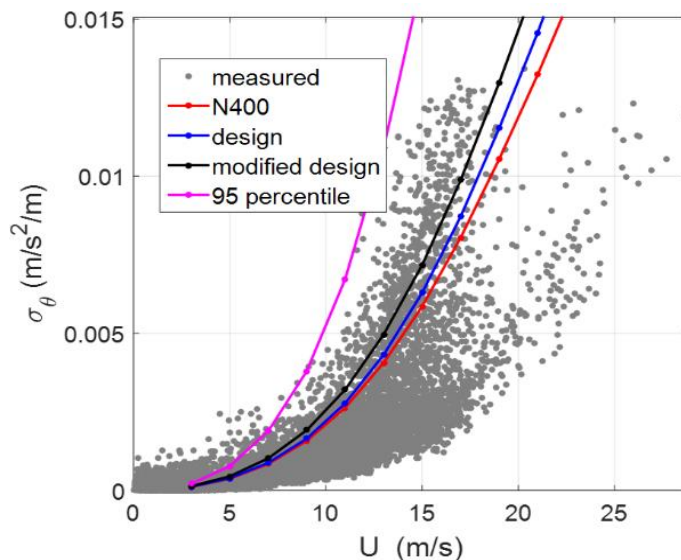
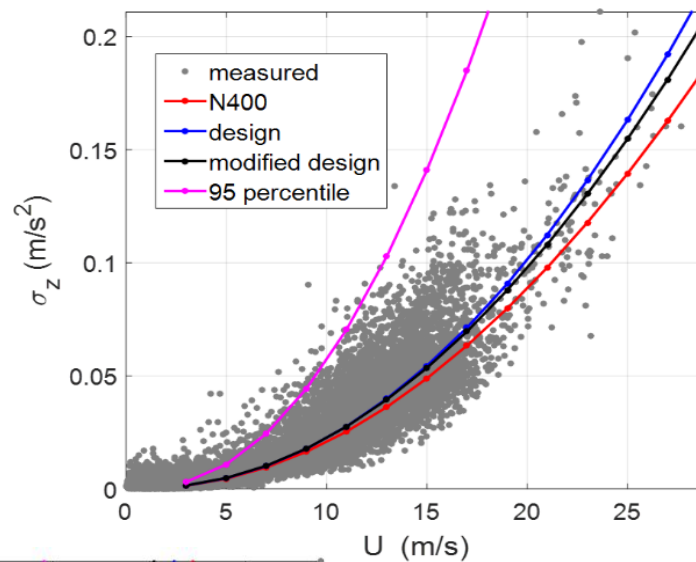
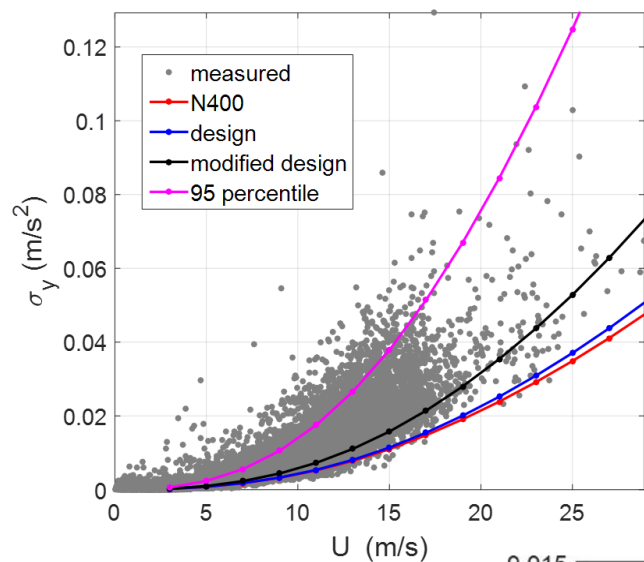


- ADs & static coefficients → wind tunnel tests
- 4 cases

Analytical Prediction of the Buffeting Response

- N400
 - Suggested expressions were used directly
- Design basis
 - N400 adjusted using field measurements
- Modified design
 - Modified using full-scale data
 - Turbulence intensity, one- point spectra, coherence (mean values)
 - Static coefficients corresponding to 3° attack angle
- Conservative
 - 95 percentile values for turbulence intensity & coherence

Analytical Prediction of the Buffeting Response



Conclusions

- Terrain is complex → variable wind conditions
- Observed variability in response doesn't agree with the design methodology
- Variability in response is attributed to the wind field
- Predictions didn't yield satisfactory design curves – why?
- Conservative approach → too conservative
- Eventually → new design approach ?

Thank you...